

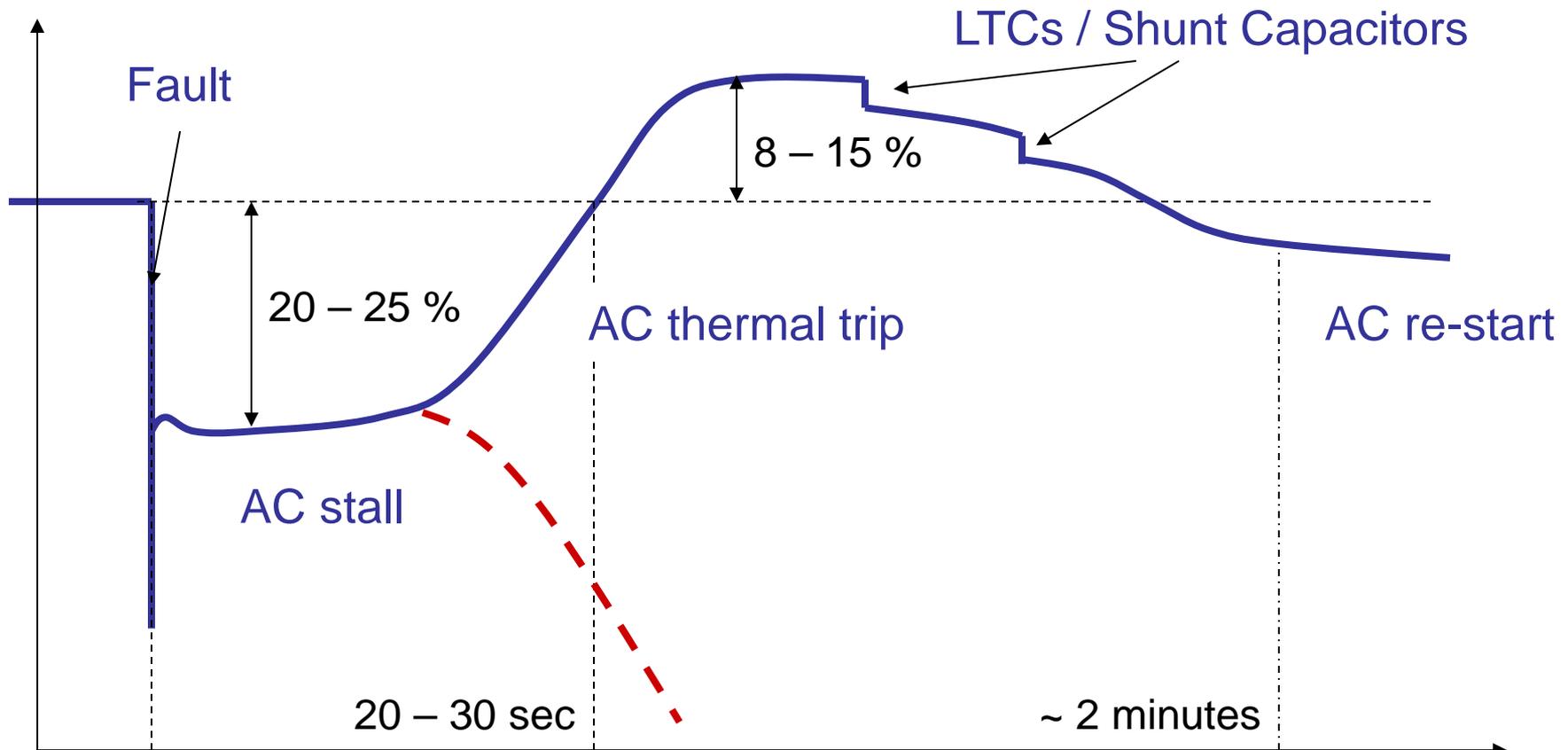
# Load Modeling in Grid Simulations and System Performance Issues

Presentation at DOE Workshop

Dmitry Kosterev  
Bonneville Power Administration  
April 2008

# Delayed Voltage Recovery Event

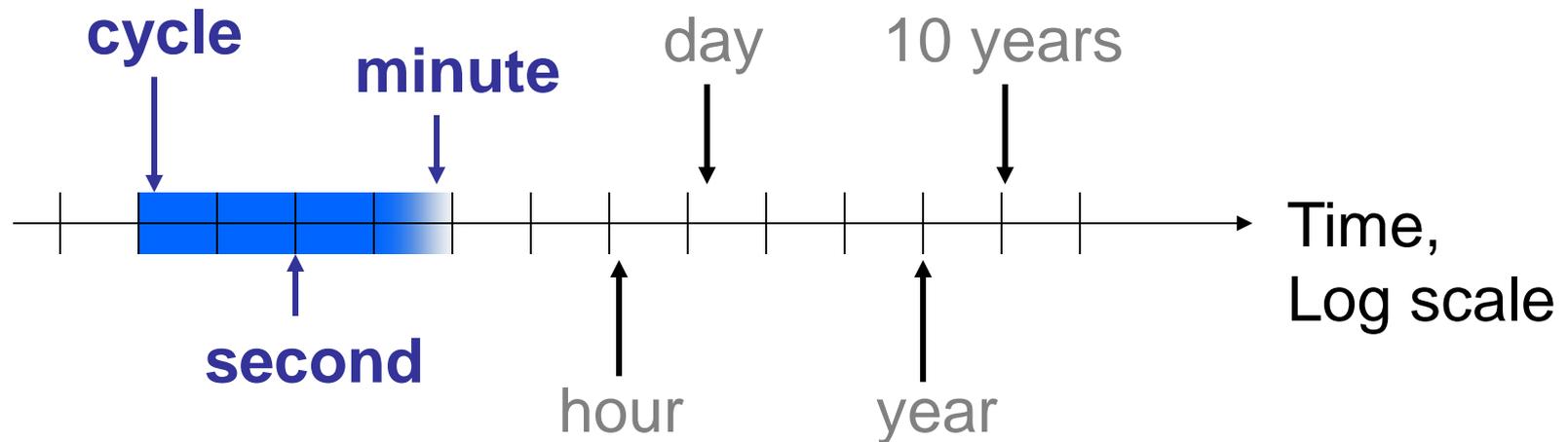
Main Grid Voltage



# Load Modeling

## Timescale of Interest

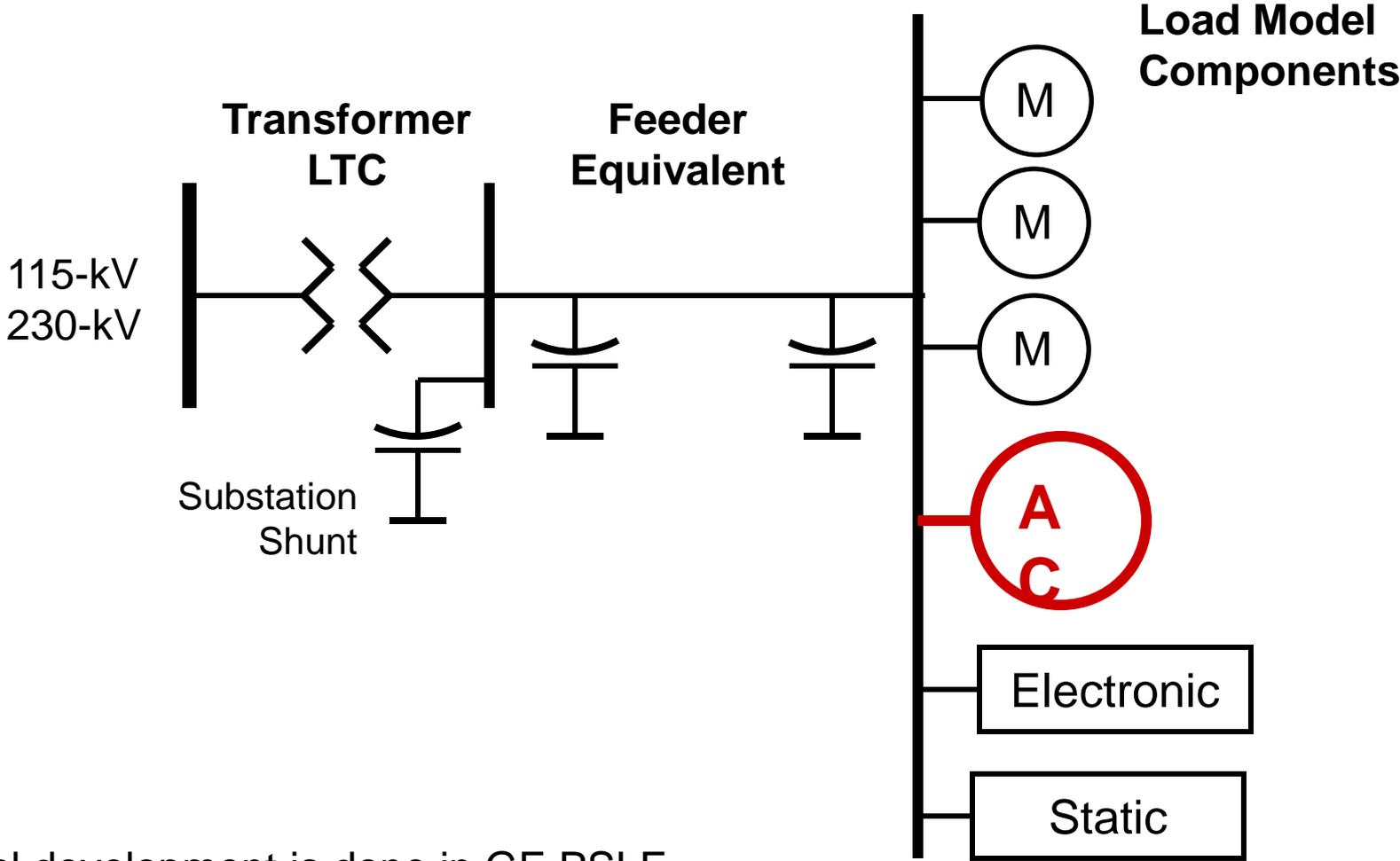
Our primary interest is the fast dynamic response of loads, not projections of future demand.



# Load Modeling in WECC

- Load Model Structure:
  - Composite load model in WECC production programs
  - Explicit load representation
- Load Model Data
- System Impact Studies:
  - Sensitivity, Validation, System Performance

# WECC Composite Load Model



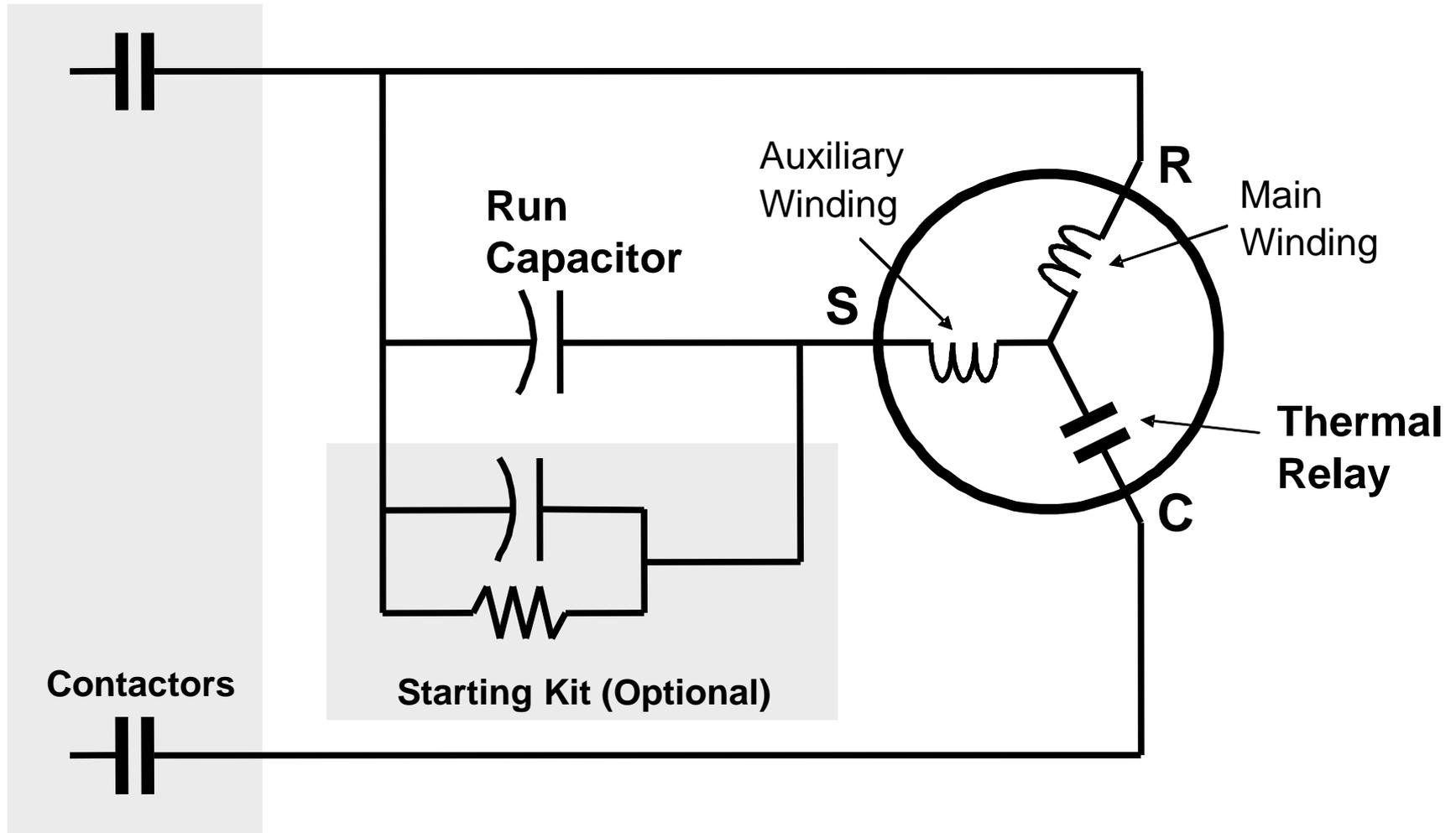
Initial development is done in GE PSLF

# Load Model Structure

- WECC developed EPCL routines for explicit load representation in PSLF program in 2004–05:
  - Add Transformer
  - Add Feeder Equivalent
  - Create Load Composition
- WECC developed a user-defined model of single-phase residential air-conditioners
- WECC is working with GE on developing a composite load model in PSLF program
  - Specifications are developed in March 2006
  - Several releases have been tested since April 2007
  - Final version is expected in Q1 of 2009

# **Single-Phase A/C Compressor Motor Model**

# A/C Compressor Motor



1-phase motor has 2 windings

# Single-Phase Motors – Steady-State

(a) Compressor motor in a 3-ton air-conditioning unit

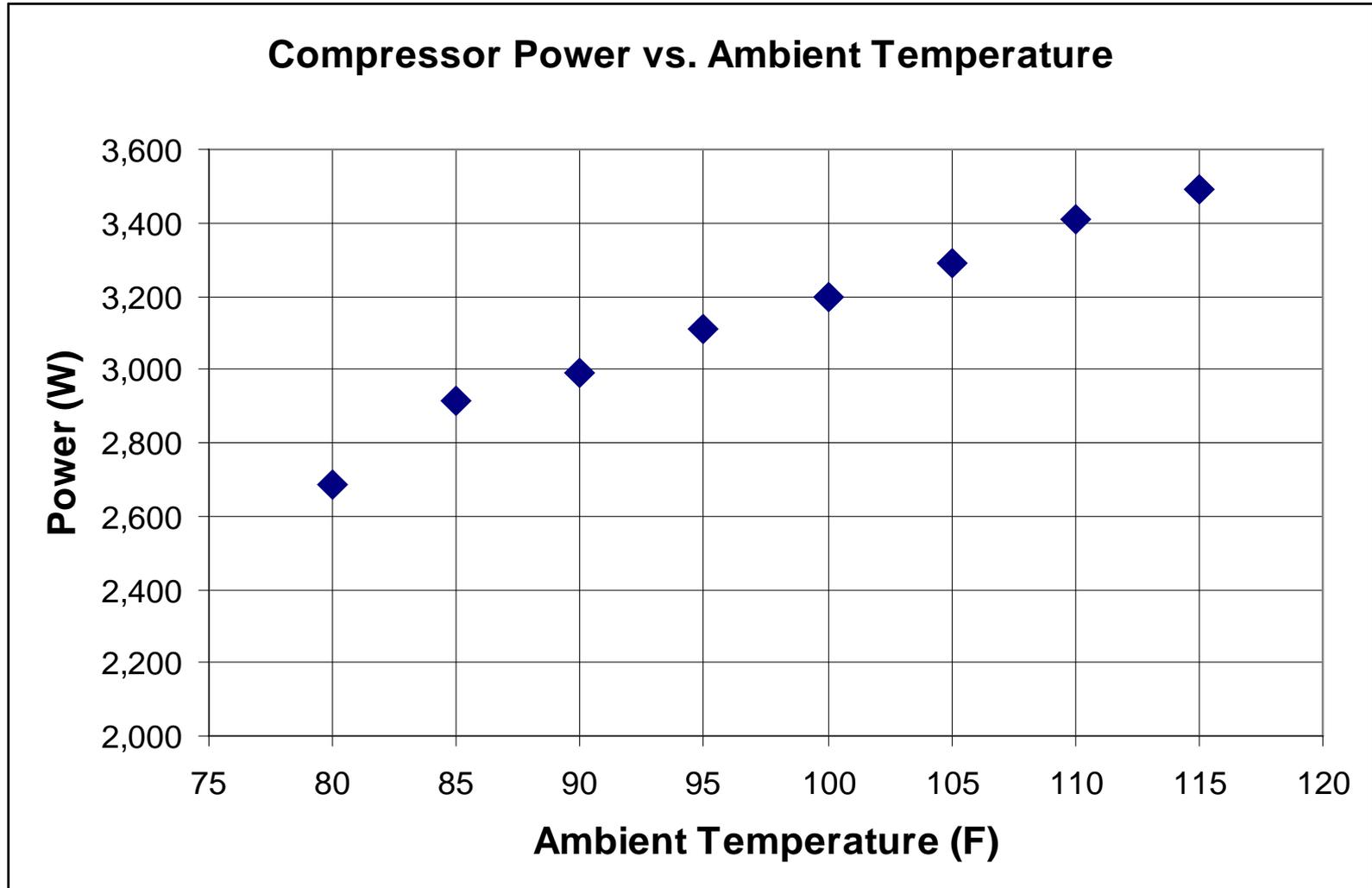
	Total	Main	Auxiliary(*)
Real Power, W	3180	1910	1270
Reactive Power, VAR	730	1645	-915
Power Factor, Per Unit	0.974	0.758	-0.81

(b) Compressor motor in a 3.5-ton air-conditioning unit

	Total	Main	Auxiliary(*)
Real Power, W	3790	2500	1290
Reactive Power, VAR	800	2000	-1200
Power Factor, Per Unit	0.978	0.781	-0.732

Notice high power factor

# Single-Phase Motors – Steady-State



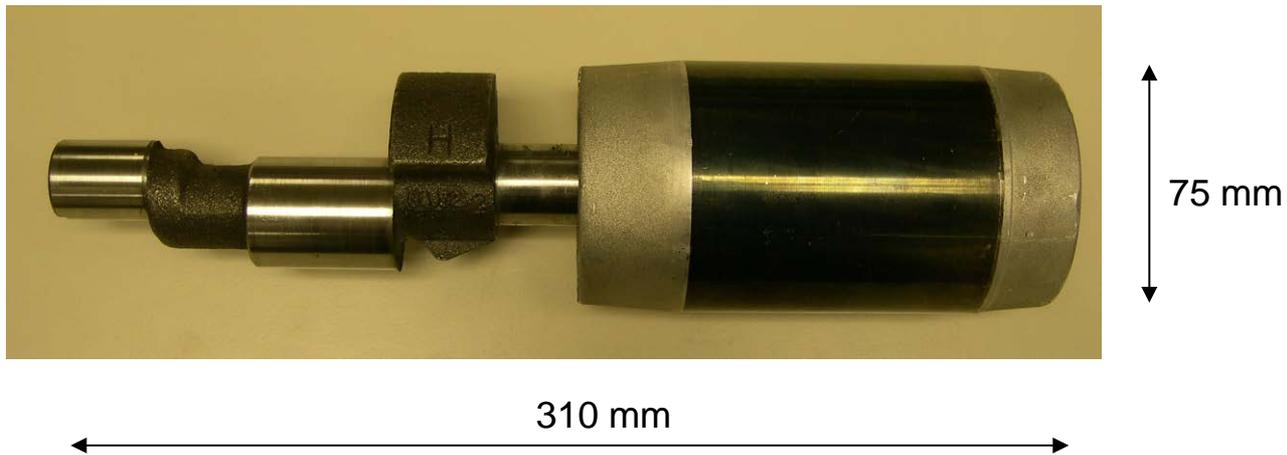
3-ton compressor motor

# Compressor Motor Tests – Motor Inertia

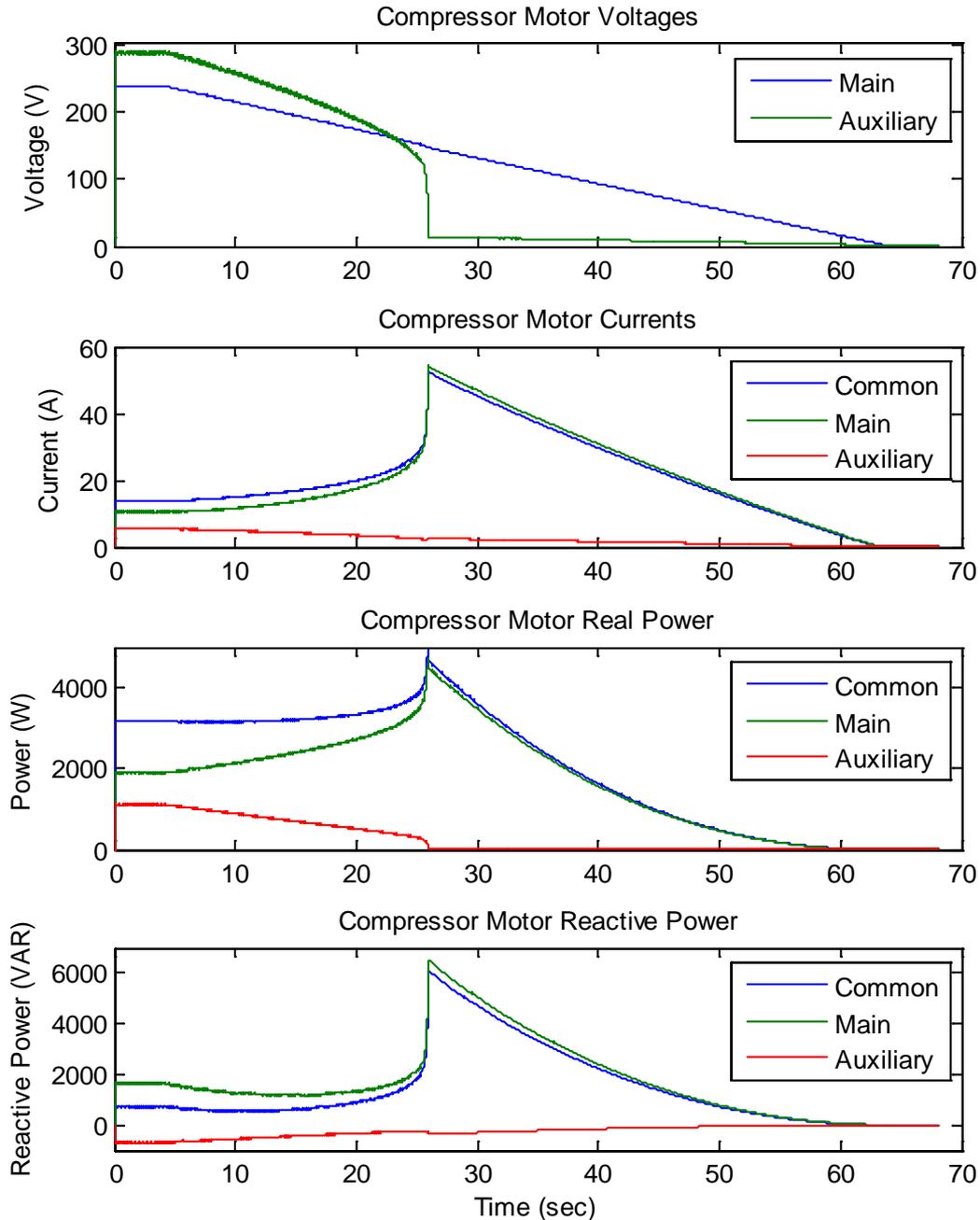
$$H = 0.03 - 0.05 \text{ seconds}$$

E.g. 3.5-ton compressor motor:

Weight: 4.6 kg

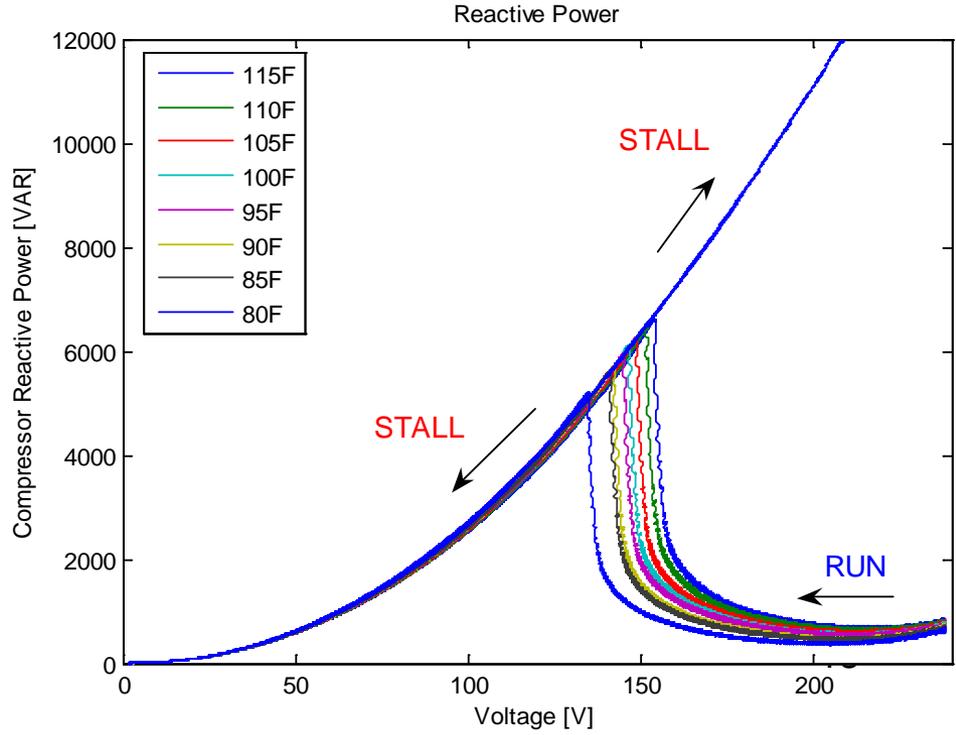
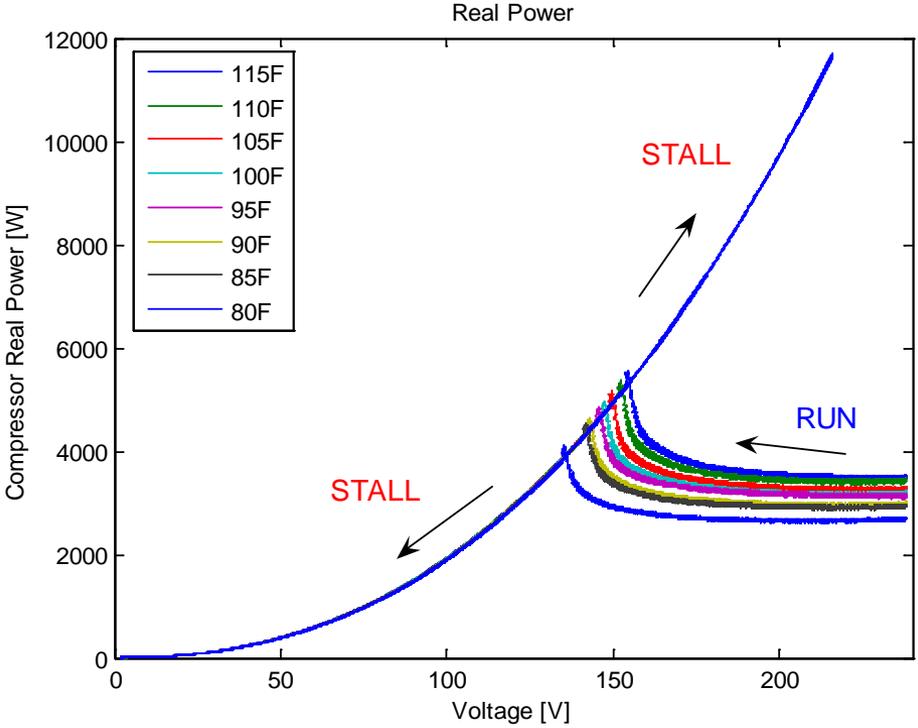


# Compressor Motor Tests – Voltage Ramp



Notice motor non-symmetric behavior becomes more pronounced as voltage ramps down

# Compressor Motor Tests – Power-Voltage Trajectories



Notice that stall voltage increases with temperature

# 1 $\phi$ – AC Motor Tests

- Compressor motor is 1-phase capacitor-run motor, has 2 windings
- Nominal power factor is relatively high 0.95 – 0.97
- Compressor load and stall voltage increase with temperature
- Compressor motor inertia is very low (~0.05 sec)
- Compressor motor is non-symmetric, non-symmetry becomes more pronounced as voltage declines
- Once the motor stalls it is likely to remain stalled until coolant pressure is equalized, very few motors can re-start

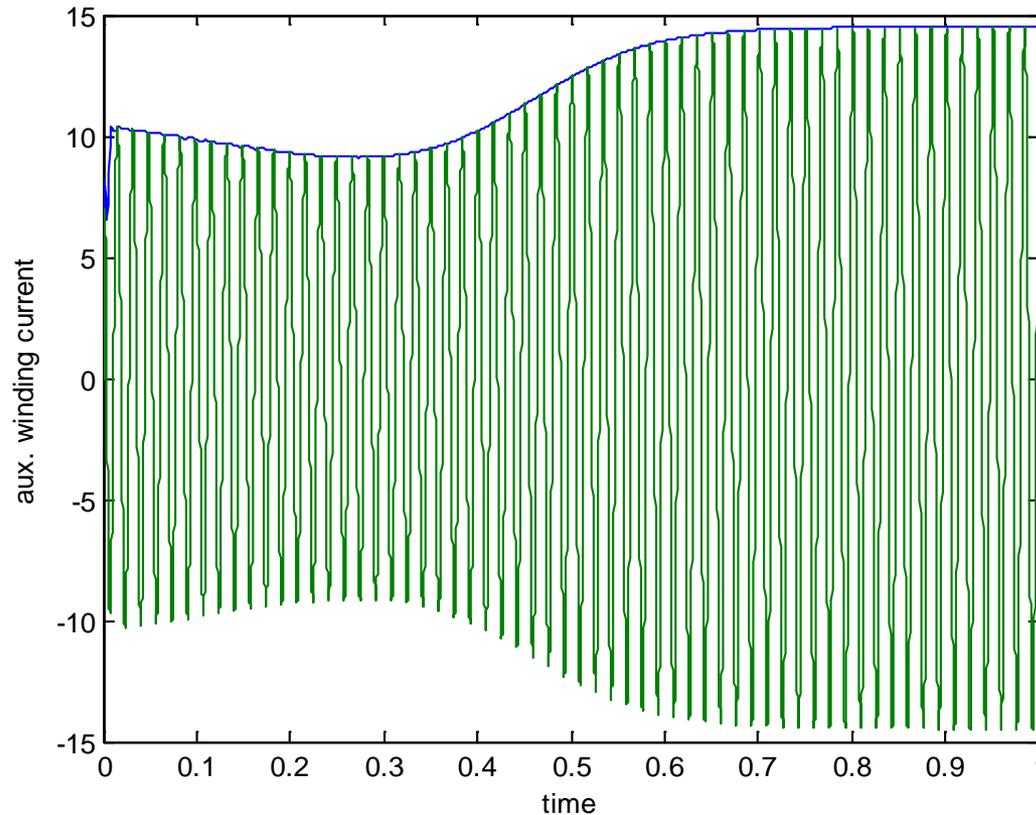
# Single-Phase Motor Models

- Three-phase motor models cannot represent behavior of single-phase motors:
  - Stalling phenomenon (3-phase motor model usually stalls at much lower voltages)
  - Real and reactive power when stalled
  - Steady-state sensitivities of real and reactive power with respect to voltage and frequency
- Single-phase motor models exist but require point-of-wave simulations
  - Not acceptable for positive-sequence grid simulators which use  $\frac{1}{4}$  cycle time step

# Single-Phase Motor Models

- Phasor Models
- Performance-Type Models
  - Several variations
- Hybrid model
  - Originally developed by SCE, enhanced by EPRI
- Single-Phase Waveform Conversion

# Phasor Model\*



\* This model was developed by Bernard Lesieutre at LBNL, and his research was funded by California Energy Commission's Public Energy Research Program, WA# MR-049, through the California Institute for Energy and Environment, Award Number MTX-060-1.

# Phasor Model

- Can be simulated with  $\frac{1}{4}$  cycle time step used in the grid simulators
- Uses differential equations to represent motor dynamics
- Matches well most tests:
  - Voltage steps, ramp, oscillations
  - Frequency steps
  - Correctly identifies faults when compressor motor stalls from the faults when compressor motor re-accelerates

# Phasor Model

- Outstanding research issues:
  - Torque model: Simulated inertia had to be reduced to about  $\frac{1}{2}$  of the measured to reproduce motor stalling. This may be because the torque of a reciprocating compressor is not modeled appropriately when the motor stalls. Higher inertia fits well with the oscillation tests. Bernie plans to repeat the tests for a scroll compressor.
- Outstanding implementation issues:
  - John Undrill is working on “motorc” model in GE PSLF. Still, need to reconcile Bernie’s MATLAB model and John’s “motorc” model

# Phasor Model

- The model has been useful in developing understanding of single-phase motors. The model will be a valuable addition to grid simulators as a stand-alone model to study specific motor behavior.
- The model, however, may not be the best choice for grid-level studies, as the model precision is lost when representing an aggregate behavior of multiple motors in a feeder.

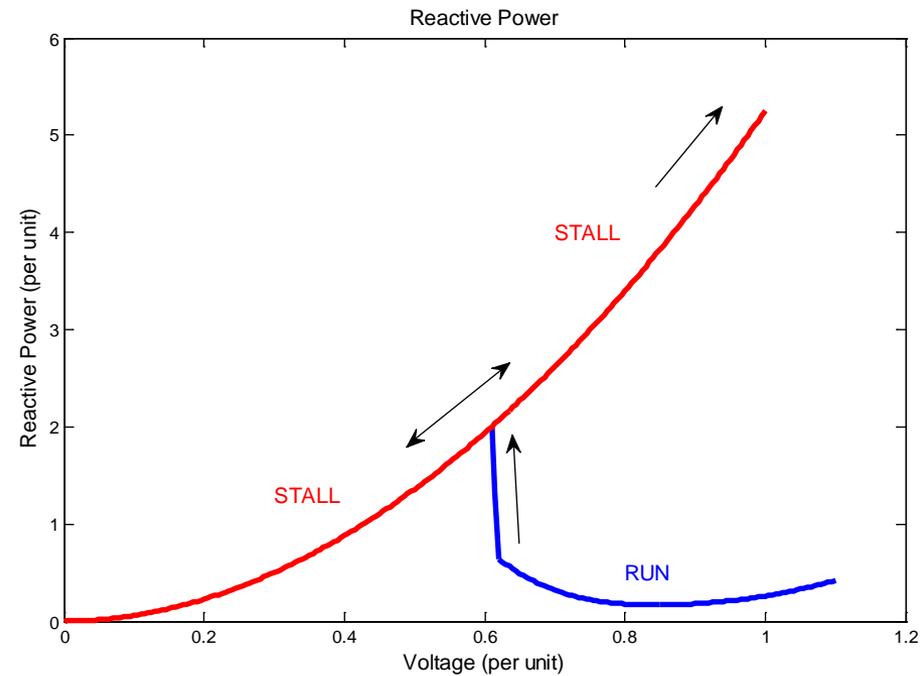
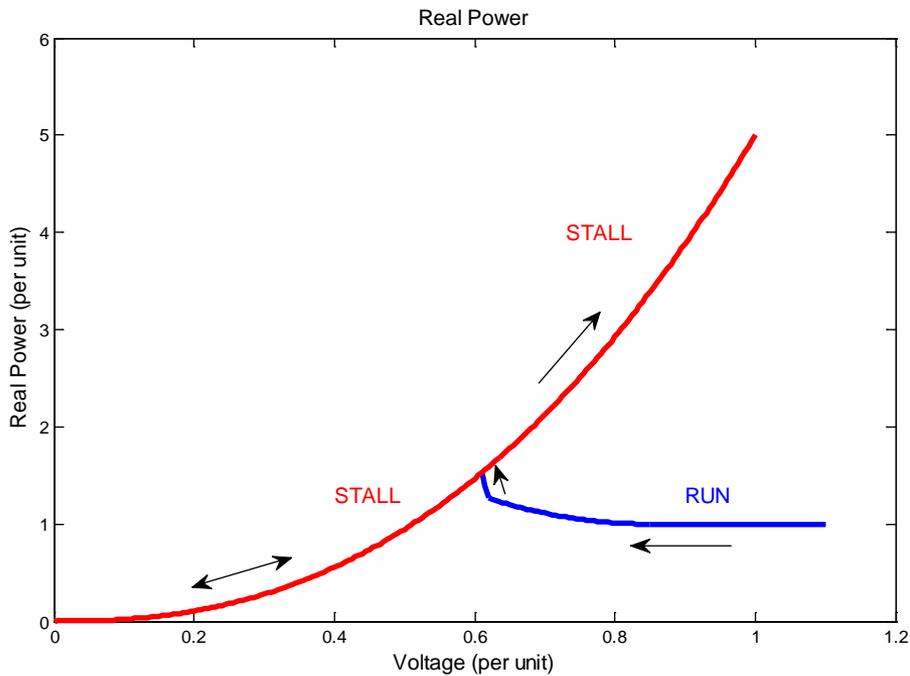
# AC Motor Model

- Grid-simulation model
  - Simulation of the impact of air-conditioning loads on the grid dynamic performance
- Equipment model
  - Gain the insight in the dynamic behavior of air-conditioning units
- Coordination and cross-calibration of the models

# Performance-Type Models

- The model has two states: running and stalled
- The transition from running to stalled state is done based on the motor voltage
- Running state is represented with static exponential models
- Stalled state is represented with an equivalent impedance  $R_{STALL} + j X_{STALL}$

# BPA Performance Model



Characteristics and stall voltage are adjusted depending on the motor load factor

# Performance Model

- Easy to implement
- Model provides good representation of the motor real and reactive power for slow variations of voltage and frequency
- Model does not capture well voltage and frequency dynamics above 0.7 Hz.
- Model is “happier” to stall than the actual motor
- Model captures well motor current, real and reactive power during the stall condition

# 1 $\phi$ - AC Unit Model

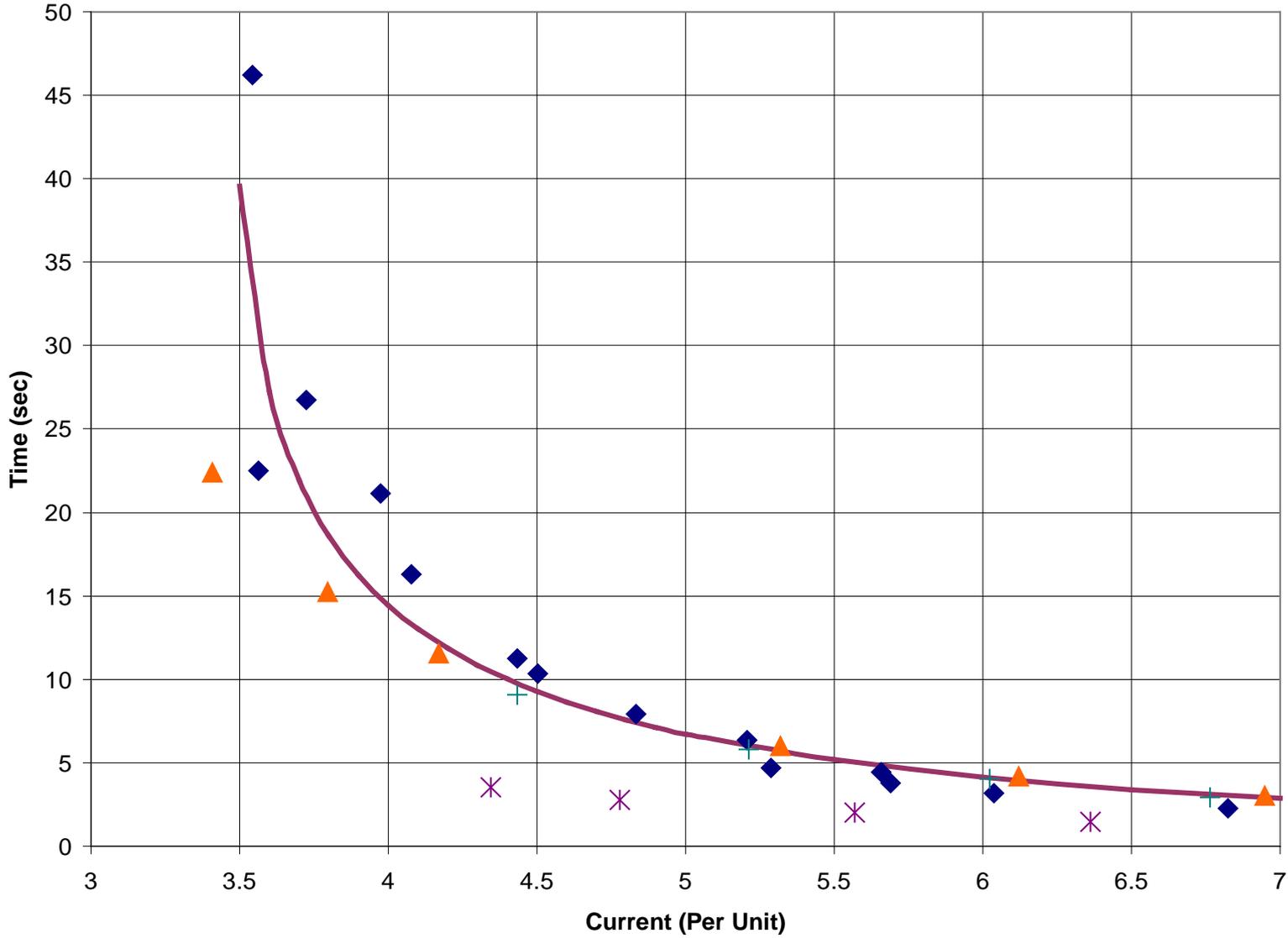
Model Includes:

- Compressor Motor Model
- Thermal Relay Model
- Under-Voltage Relay (proposed by SCE) Model
- Condensing Unit Controls / Contactors

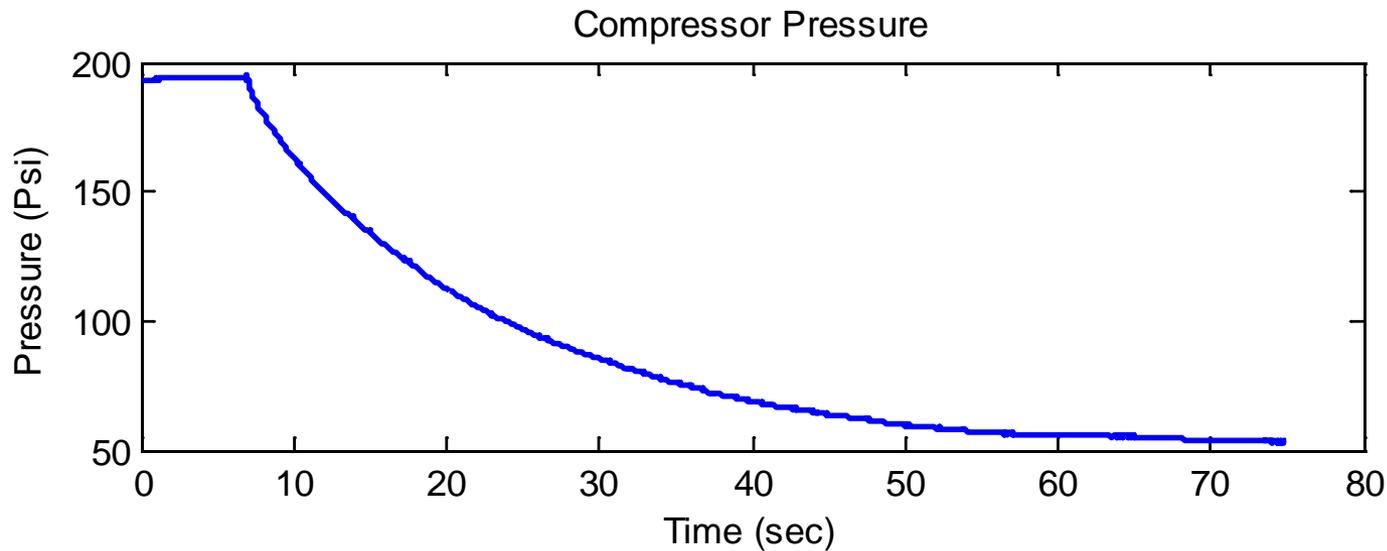
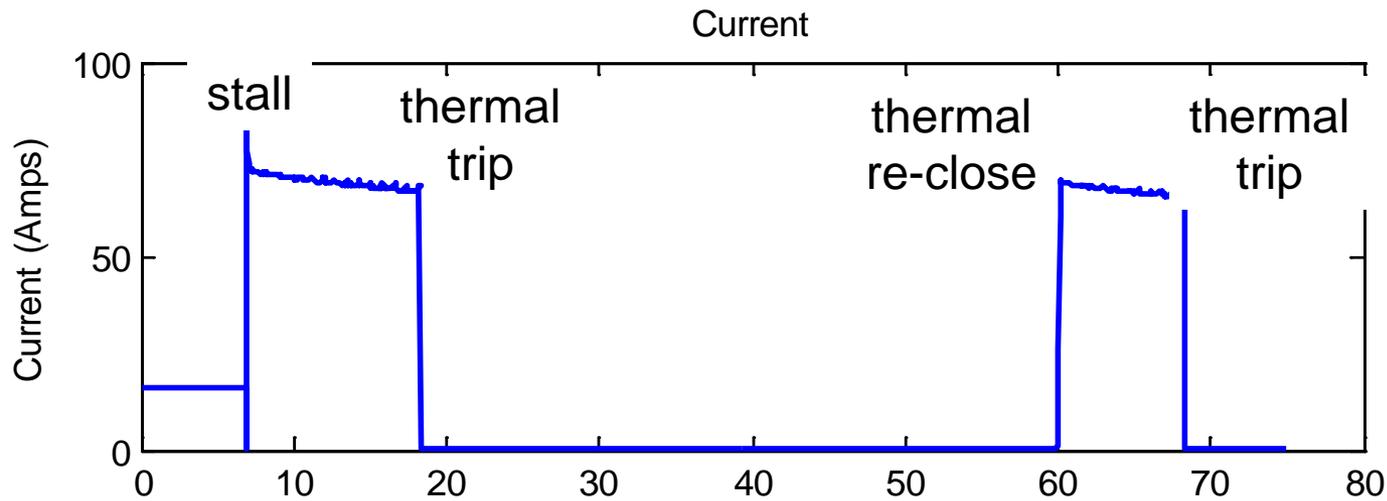
Model Does NOT Include:

- Indoor and Outdoor fans are modeled separately

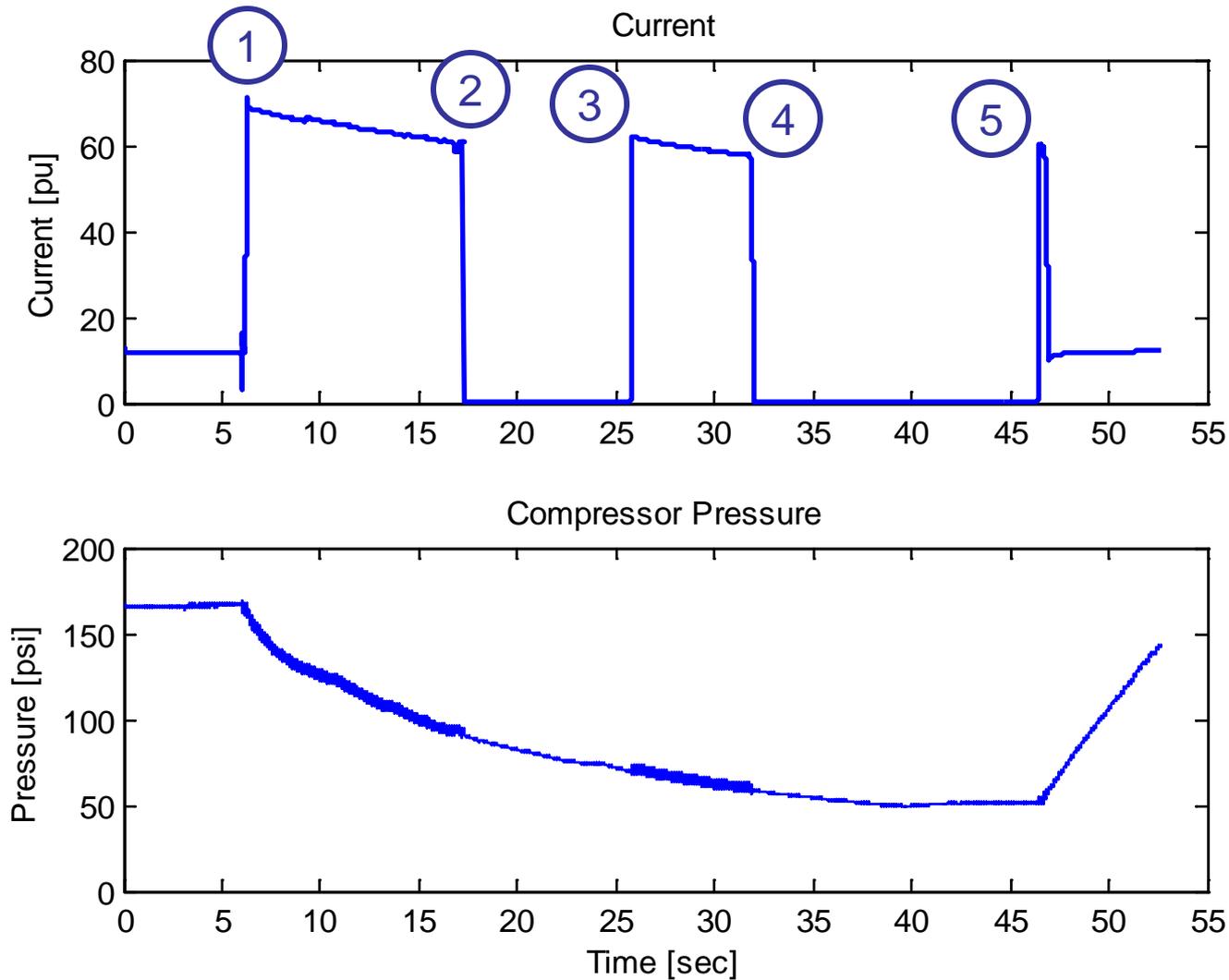
# Thermal Relay Characteristic



# Thermal Protection



# Thermal Protection

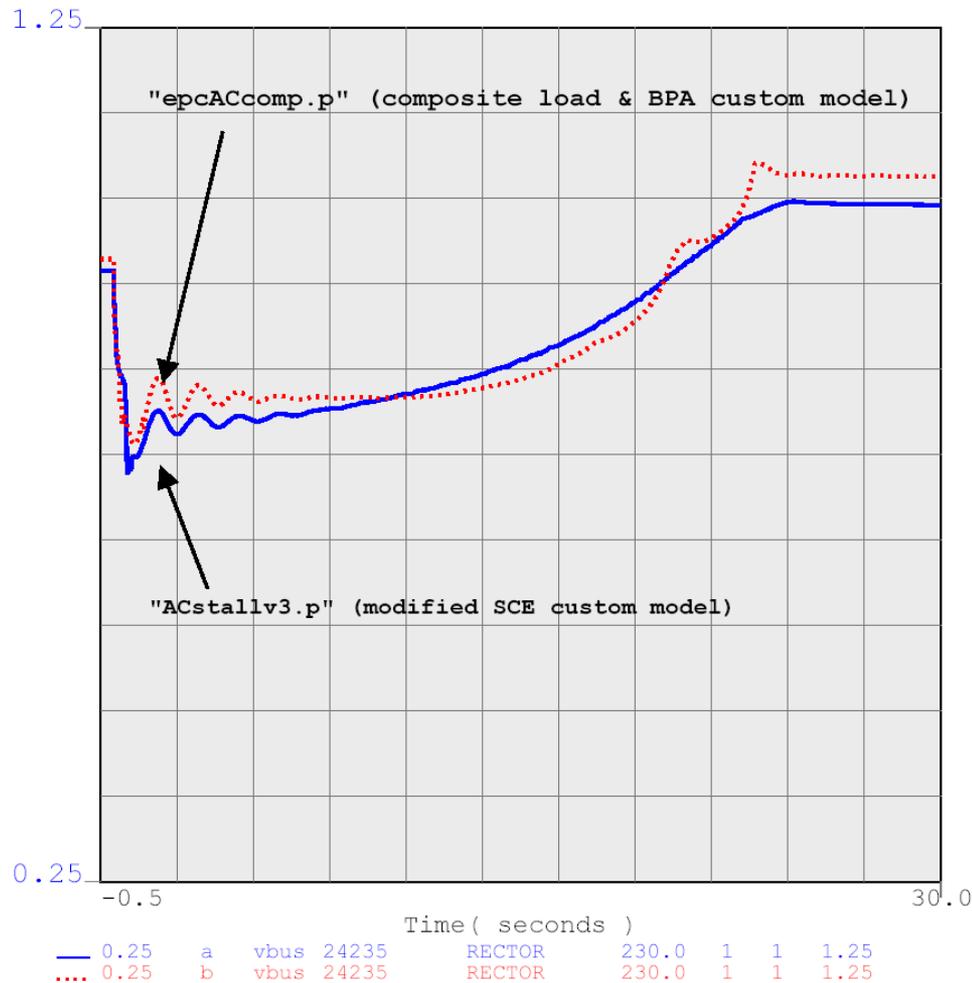


# WECC Status

- AC-Motor Model Development:
  - Include “performance” – type AC compressor model in a WECC composite load model
  - Continue development of the “motorc” model as a stand-alone model in power system simulators
  - WECC is preparing a detailed report on 1- $\phi$  compressor testing and modeling
- Composite load model is expected to be done in Q1 2009:
  - Prototype is currently available in GE PSLF 16.1
  - Outstanding development – 1-phase motors, connect to UVLS and UFLS data records
  - Model acceptance tests and system performance studies
  - Load composition data

# Load Model Studies

# Load Model Studies



Explicit load representation

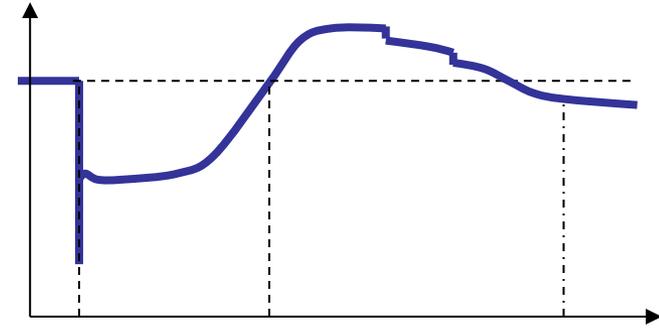
“Performance” model for 1phase A/C units

Simulations done by Robert Tucker, SCE

# System Studies

- AC Units Stall:

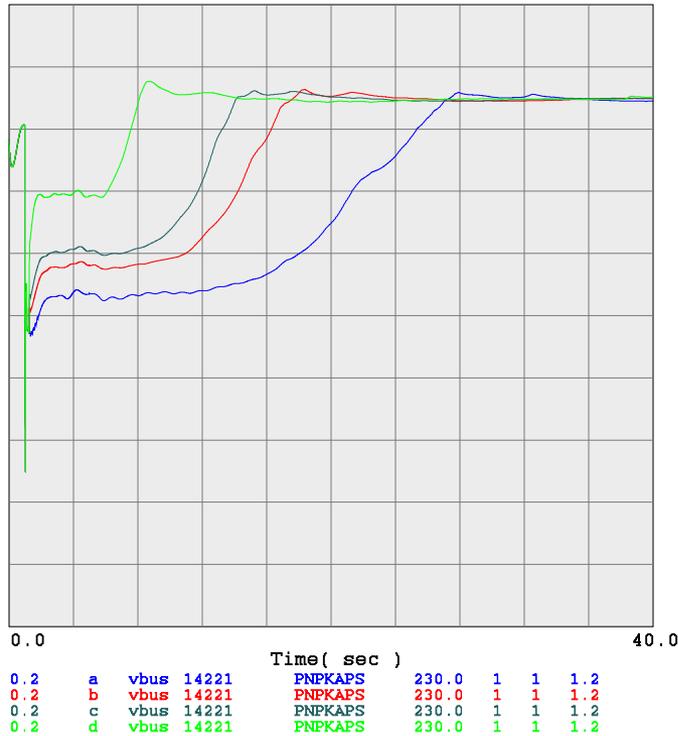
- A grid fault turns into a “wide-area” fault
- Represents a risk to voltage stability
  - Risk of generator reducing reactive power by OEL
  - Risk of operation of Zone 3 protection
- Need to disconnect stalled AC units from the grid
- Need to contain the affected area



- AC Units are disconnected:

- “Your risks can change rapidly”
- Risk of major over-voltages, equipment damage and protective tripping
- Dynamic reactive resources help

# Studies of Solutions



3-phase fault

Hassayampa – Palo Verde

Normal clearing

Explicit load representation

“Performance” A/C model

Residential AC is 30% of load

Baseline simulation

20% of a/c tripped by UV relay

30% of a/c tripped by UV relay

60% of a/c tripped by UV relay

TASMO MODEL; OUTPUT GENERATED 2002-07-16 11:52:05  
SWINGBUS 1520 FOR FC-2001-1:2003-07-14:17:4F--1--1-0-0  
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# Our Viewpoint

- Large metro areas:
  - Increasing amount of air-conditioning load
  - Limited dynamic voltage support – generators are remote and VARS do not travel well
  - Prone to dynamic voltage stability problems
- BPA view of the risks:
  - Risk of voltage collapse developing in a metro area
  - Risk of voltage collapse cascading outside metro area
  - Risk of extreme over-voltages
- Solutions:
  - Equipment-level solutions
  - System solutions – dynamic VARs are needed
  - Special Protection Schemes to prevent outage spread

# Acknowledgement

- WECC composite load model is a collaborative development of many researchers, including
  - Bill Price and John Undrill, retired from General Electric
  - Anatoly Meklin, Pacific Gas and Electric
  - Bernie Lesieutre, LBNL, University of Wisconsin
  - Richard Bravo, Garry Chinn, Robert Tucker – Southern California Edison
  - Steve Yang and Frank Puyleart – Bonneville Power Administration
  - Irina Green – California ISO
  - Donald Davies, WECC Staff
  - Orlando Ciniglio – Idaho Power Company
  - Donald Sutphin, VIASYN
  - Peter Mackin, Navigant Consulting
- AC Modeling Research:
  - California Energy Commission's Public Energy Research Program, WA# MR-049, through the California Institute for Energy and Environment, Award Number MTX-060-1
  - BPA Technology Innovation Office